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(71) Applicant(s)
Vision Systems Limited

(54) Inventor(s)
Martin Terence Cole

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57636

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(1) MARTIN TERENCE COLE
of C/o IEI (Australia) Pty. Ltd.,
29 Stafford Street,
Huntingdale, Victoria 3165.
Australia.

(2) Here
Insert Title
of Invention.

hereby apply for the grant of a Patent for an invention entitled: (2)
IMPROVEMENTS RELATING TO SOLID-STATE ANEMOMETERS
AND TEMPERATURE GAUGES

which is described in the accompanying PROVISIONAL specification.
~~COMPLETE~~

My
~~our~~ address for service is Messrs. Edwd. Waters & Sons, Patent Attorneys,
50 Queen Street, Melbourne, Victoria, Australia.

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DATED this 8th day of May, 1984

(3) Signa-
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By

L.J. DYSON

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(1) Here
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In support of the Application made by⁽¹⁾

MARTIN TERENCE COLE

(2) Here
insert title
of Invention.

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IMPROVEMENTS RELATING TO SOLID-STATE ANEMOMETERS

AND TEMPERATURE GAUGES

(3) Here
insert (in
full) Address
or Addresses.

of⁽³⁾ c/ IEI (Australia) Pty. Ltd., 29 Stafford
Street, Huntingdale, Vic. 3165.

do solemnly and sincerely declare as follows:

1. I am
XXXXXX the applicant for the patent.

2. I am
XXXXXX the actual inventor of the invention.

or

2. ⁽⁴⁾

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insert full
Name(s) and
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of Actual
Inventor(s) if
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the actual inventor of the invention, and the facts upon which I am
entitled to make the application are as follows

XX

XXXXXXXXXXXXXXXXXXXX I am XXX

(5) Full Name
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Inventor or
Inventors.

XXXXXX the assignee of the said Pat.

DECLARED at Huntingdale
this Twenty Fourth day of April 1984

(6) Signature
of Applicant or
Applicants.

(6)

(12) PATENT ABRIDGMENT (11) Document No. AU-B-42298/85
(19) AUSTRALIAN PATENT OFFICE (10) Acceptance No. 576361

(54) Title
SOLID STATE ANEMOMETER AND OPTICAL AIR POLLUTION MONITOR

(51)4 International Patent Classification
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(71) Applicant
MARTIN TERENCE COLE

(72) Inventor
MARTIN TERENCE COLE

(74) Attorney or Agent
EDWD. WATERS & SONS

(56) Prior Art Documents
51180/73 480589 00.71, 56.64
57869/73 480813 00.71, 88.2

(57) Claim

1. A solid state anemometer comprising:

(A) a differential temperature measurement circuit including:

- i. a bridge circuit
 - ii. A source of bias supply connected to opposite corners of said bridge circuit thereby to define two branches in shunt to said bias supply;
 - iii. each branch having in series a current limiting resistor and a Zener diode poled so that its P-N junction is back-biased by said supply; and
 - iv. means for connecting the conductor between said current limiting resistor and the associated Zener diode of each branch to respective output circuits whereat a differential output voltage can be sensed;
- the values of said current limiting resistors and the breakdown voltage-current characteristics of said Zener diodes being substantially identical; the voltage of said bias source being sufficient to cause a reverse breakdown of substantially equal value to flow through each of said Zener diodes, whereby when the temperature of said two Zener diodes is substantially the same over a considerable range of ambient temperatures the said differential output voltage is substantially negligible; and whereby, as the

temperature difference between said Zener diodes increases over said considerable range of ambient temperatures, said differential output voltage varies substantially and correspondingly in linear relation to said temperature difference; wherein both said Zener diodes are under the thermal influence of a fluid, one of said Zener diodes being exposed to the thermal influence of a fluid flow and the other Zener diode being isolated from said fluid flow, whereby the heat developed by the reverse breakdown current through each Zener diode is dissipated differently because of the difference in fluid flow; and

(B) means for measuring the differential output voltage, if any, existing between said diodes caused by the cooling effect of said fluid flow, if any, said measured differential being an indication of fluid flow speed.

4. An optical air pollution monitor, said monitor including a solid state anemometer according to claim 1 which is used as an air flow detector, one of the Zener diodes of said anemometer being exposed to a fluid flow in said monitor, said fluid being sourced from an area under surveillance, the other Zener diode of said anemometer being isolated from said fluid flow but being in fluid having substantially the same temperature as the area under surveillance, said differential output voltage being an indication of continuous fluid sampling by said air pollution monitor from said area under surveillance.

576361

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Form 10

PATENTS ACT, 1952-69

COMPLETE SPECIFICATION

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Complete Specification Lodged:
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Priority:

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42298/85

Name of Applicant: MARTIN TERENCE COLE

Address of Applicant: c/o IEI (Australia) Pty. Ltd.
29 Stafford Street
Huntingdale, Victoria 3165
Australia

Actual Inventor: MARTIN TERENCE COLE

Address for Service: EDWD. WATERS & SONS,
50 QUEEN STREET, MELBOURNE, AUSTRALIA, 3000.

Complete Specification for the invention entitled:

"IMPROVEMENTS RELATING TO SOLID-STATE
ANEMOMETERS AND TEMPERATURE GAUGES"

The following statement is a full description of this invention, including the best method of performing it known to us

IMPROVEMENTS RELATING TO SOLID-STATE
ANEMOMETERS AND TEMPERATURE GAUGES

The present invention relates to a solid state anemometer or a temperature gauge and in particular to anemometers for use in air-pollution monitoring techniques.

The anemometer is an instrument for measuring the speed of air, whether for meteorological data, ventilation testing or other purposes. The majority of anemometers comprise some form of impeller which rotates due to air movement. The speed of rotation is calibrated to provide a measure of air velocity. Such anemometers consist of mechanical parts and consequently are costly to manufacture, are subject to wear and damage which reduces service life, and are difficult to miniaturize. Furthermore, because energy must be imparted to the impeller to overcome frictional losses, there is a restriction to flow when mounted within pipes.

More recently, solid-state anemometers have been developed for use in ventilation testing. These utilize a pair of thermistor bead elements wired as a compensating circuit (see schematic, Fig. 1). It should be noted that the thermistors are passing current and are consequently dissipating heat, placing each thermistor at a modestly elevated temperature relative to ambient. This is essential so that air flow may cause cooling of the sampling thermistor. One thermistor is exposed to the air flow (sampling element), whilst the other thermistor is protected in still air at ambient temperature (reference element). Ideally, under conditions of zero air speed, the thermistors operate at equal temperatures and thus, the resistance value of each thermistor is equal and the compensating circuit is in balance (zero differential output). When air flows, the sampling thermistor is cooled, which alters its resistance value, causing the circuit to become unbalanced. Accordingly the differential output voltage from the circuit can be calibrated in terms of air flow. The intention of the

reference thermistor and the compensating circuit is to allow the anemometer to compensate for variations in ambient temperature. However the accuracy of this compensation has been poor, requiring manual adjustment of the zero setting before each series of air speed measurements is taken. In a hand-held anemometer, this is an inconvenience but not a major problem.

Further disadvantages of thermistor beads have been experienced. The fine connecting wires are subject to damage, fatigue and corrosion, whilst the bead resistance has exhibited a susceptibility to ageing. In addition, thermistor beads are quite expensive and are very difficult to handle during anemometer assembly.

A new application for anemometers has given rise to a new method for measuring air speed, which provides adequate compensation for temperature drift and is compact, robust, inexpensive, simple to manufacture, contains no moving parts, is miniature and provides negligible restriction to air flow.

An optional air-pollution monitoring technique has been adapted for the purpose of detecting the earliest traces of smoke from incipient fires, thereby to reduce the loss of life and property caused by established fires. This is especially applicable to situations where modern synthetic materials may become involved, because of the highly toxic fumes liberated.

It is required that representative samples of the air within each part of the fire detection zone, be passed through the smoke detector, such that the air quality can be continuously monitored. Such monitoring may be achieved by a mechanically-aspirated pipe network or more simply, by coupling to the return-air register of an air-conditioning system.

In either case, any interruption to the air flow through the smoke detector must be detected, lest a dangerous fire remain undetected.

In the pipe network case, the possible restriction to air flow caused by an anemometer is an important

consideration, since an aspirator of minimum energy input is necessary, to enable continued operation from modest-capacity standby batteries, in the event of mains failure.

A solid-state anemometer is known utilizing a thermistor compensating circuit to detect a loss of air flow, thence to create an appropriate alarm signal. However such an insitu anemometer must be capable of compensation for wide variations in ambient air temperature, in many of the applications of the smoke detector.

10 Description of Prior Art

Reference will be made to Figures 1 to 3 illustrating known thermistor circuits and graphs of differential output voltages plotted against temperatures.

15 The graphs of Fig. 1 show the differential output voltage from a compensating circuit, consisting of a typical pair of precision thermistors. Under conditions of zero air flow, the differential output voltage is markedly dependent upon temperature. This dependence becomes yet greater, under conditions of maximum air flow (as determined by the given pipe network and aspirator). The vertical voltage excursion between these two curves, at any given ambient temperature, represents the response of the thermistor anemometer to all air speeds between zero and maximum.

20 The switching threshold, below which the alarm signal is to be generated, has been placed for convenience and is normally adjustable. This threshold switching function is normally achieved by means of a comparator circuit. At the typical ambient temperature of 20°C for example, the alarm would be generated should the differential output voltage fall to about one-third of the possible voltage excursion. It should be noted that because of the non-linear response of the thermistor anemometer to air speed, this one-third voltage could represent an air speed of only 10 to 20% of the maximum.

35 Such a span of operation would be acceptable, provided the ambient temperature deviation was small, in the region of 5 to 10°C (e.g. air-conditioned area).

However, should the ambient temperature rise by 20°C or more, it would become impossible to exceed the alarm threshold and an alarm signal must be generated, irrespective of air speed. Furthermore, should the ambient temperature fall by 20°C or more, it would become impossible to reach the alarm threshold and an alarm signal could not be generated, irrespective of air speed. For practical purposes, the full span of operation of such an anemometer would be rather less than 40°C, rendering it unsuitable for areas which are exposed to seasonal temperature changes. To factory-set the alarm threshold, without knowledge of the product destination, would be largely pointless.

More significantly, the use of dust filters in association with the smoke detectors has led to a requirement for sensitive setting of the alarm threshold, according to the actual flows achieved in the field, such that the partial-blocking of the filter can be detected. It is not sufficient merely to detect a total air flow loss. To detect for example, a 30% loss in flow, accurately across a range of -20°C to +50°C, requires a substantial jump in the accuracy of temperature compensation.

The reason for the poor performance of the thermistor design can be readily understood by reference to Figure 2 of the drawings which shows the individual output voltages from each thermistor, versus bead temperature of each thermistor, assuming a supply voltage of 15V DC and a series resistor of 2k Ohm. Curves A and B represent the worst-case tolerance extremities for the precision thermistors used.

Fig. 3 illustrates the differential output voltage of a compensating circuit comprising thermistors A and B. In the case where A and B are maintained at the same temperature, the differential output voltage (A-B) is relatively flat. This represents the zero air flow situation. In the case where two identical thermistors are chosen (A-A) or (B-B), the curve would be a horizontal straight line at zero volts. However if one thermistor is exposed to air flow,

such that its temperature is reduced by 20°C below the other for example, a very steep curve (A-B) results, even when perfectly matched thermistors are used (A-A) or (B-B).

In summary, under conditions of imperfectly matched thermistors, the temperature drift relative to flow signal (differential voltage), at an ambient temperature of 20°C and high air flow is about 1.6%/°C. The difficult task of perfectly matching the thermistors would afford no improvement.

The reason for this poor performance is a fundamental limitation of the thermistor approach. Namely, it is the inherent non-linearity of the resistance vs. temperature curve. This curve is conveniently expressed in the form:

$$R = A \cdot \exp(K/(T+273))$$

Where R is the resistance and T is the bead temperature (Celsius). A is a constant understood to lie within the range 0.01293 to 0.03884 and K is a constant understood to lie within the range 4096 to 3681, as determined by the manufacturing process of the particular brand of thermistors chosen.

It can be seen that the dynamic resistance is a function of temperature. Because the two thermistors would operate at differing temperatures (depending upon air speed), they operate at different parts of this curve. Their dynamic resistances are different and consequently it becomes impossible for one to compensate for the other.

Intuitively therefore, any solution seemed to require temperature-sensing elements which had a linear response.

Integrated circuit temperature-sensing elements have been developed, which have a quite linear response. However, these are costly and are comparatively large, which can present difficulties in miniaturization and restriction to air flow. They also have a significant thermal time-constant. Accordingly, an element of low complexity was sought, such as a semi-conductor junction.

Forward-biased silicon diode junctions are known for their essentially linear temperature characteristic, commonly $2.2 \text{ mV}/^{\circ}\text{C}$. Accordingly they have been used in temperature measurement, although their application to air speed measurement is not previously known. Nevertheless, the forward voltage-drop of a silicon diode is approximately 0.6V, and to dissipate sufficient power to raise the chip temperature, such that adequate sensitivity to air flow would be achieved, would require substantial current flow, in the order of 100mA or more. This was unacceptable because the smoke detector as a whole must be highly energy-efficient, to enable operation from modest-capacity standby batteries, in the event of mains failure. Accordingly this avenue was abandoned.

It is an objective of the present invention to provide a solid state anemometer which is accurate, has low power consumption and is substantially independent of temperature variations over its working range.

A further objective is to provide a solid state temperature measuring instrument.

~~There is provided in one form of the invention~~
a solid state temperature measuring instrument for a fluid medium such as atmosphere including a zener diode exposed to said fluid medium and exhibiting a voltage output dependent upon temperature, and means for measuring said voltage output as an indication of temperature of said fluid medium.

In another aspect of the invention there is provided a fluid flow meter including a solid state circuit having a pair of semi-conductor junction means, one exposed to a fluid flow the other being isolated from said fluid flow, and means for measuring the respective outputs of said junction means to give an indication of fluid flow.

Conveniently said junction means are independently connected to said measuring means.

There is provided according to the present invention ~~a solid state anemometer including a pair of zener~~



There is provided according to one aspect of the present invention a solid state anemometer comprising:

(A) a differential temperature measurement circuit including:

- 5 i. a bridge circuit
- ii. a source of bias supply connected to opposite corners of said bridge circuit thereby to define two branches in shunt to said bias supply;
- iii. each branch having in series a current
- 10 limiting resistor and a Zener diode poled so that its P-N junction is back-biased by said supply; and
- iv. means for connecting the conductor between said current limiting resistor and the associated Zener diode of each branch to respective output circuits whereat a
- 15 differential output voltage can be sensed; the value of said current limiting resistors and the breakdown voltage-current characteristics of said Zener diodes being substantially identical; the voltage of said bias source being sufficient to cause a reverse breakdown of
- 20 substantially equal value to flow through each of said Zener diodes, whereby when the temperature of said two Zener diodes is substantially the same over a considerable range of ambient temperatures the said differential output voltage is substantially negligible; and whereby, as the
- 25 temperature difference between said Zener diodes increases over said considerable range of ambient temperatures, said differential output voltage varies substantially and correspondingly in linear relation to said temperature difference; wherein both said Zener diodes are under the
- 30 thermal influence of a fluid, one of said Zener diodes being exposed to the thermal influence of a fluid flow and the other Zener diode being isolated from said fluid flow, whereby the heat developed by the reverse breakdown current through each Zener diode is dissipated differently because
- 35 of the difference in fluid flow; and
- (B) means for measuring the differential output voltage, if any, existing between said diodes caused by the



- 7b -

cooling effect of said fluid flow, if any, said measured differential being an indication of fluid flow speed.

According to a further aspect of the present invention, there is provided an optical air pollution

5 monitor, said monitor including a solid state anemometer as described above which is used as an air flow detector, one of the Zener diodes of said anemometer being exposed to a fluid flow in said monitor, said fluid being sourced from an area under surveillance, the other Zener diode of said
10 anemometer being isolated from said fluid flow but being in fluid having substantially the same temperature as the area under surveillance, said differential output voltage being an indication of continuous fluid sampling by said air pollution monitor from said area under surveillance.

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~~diodes connected in a compensating circuit configuration,~~
one of said diodes adapted to be exposed to a fluid flow
the other being isolated from said fluid flow, means for
measuring the voltage differential between said diodes,
5 ~~said differential being an indication of fluid flow speed.~~

The invention will be described in greater detail
having reference to the accompanying figures in which:-

Figures 1 to 3 have already been described with
reference to prior art thermistors;

10 Figure 4 is a graph of test results on zener
diodes having a bias current set to produce a uniform power
dissipation of 80 milli watt (mW);

Figure 5 is a selector guide showing an approxi-
mate zener diode for a required temperature coefficient;

15 Figure 6 shows a representative sample of the
temperature characteristic of numerous zener diodes;

Figure 6(a) is a circuit for temperature measure-
ment;

20 Figure 7 is a graph of differential output voltage
against temperature of zener diode compensating circuit;

Figure 7(a) is a schematic diagram of a zener
diode compensating circuit;

Figures 8 and 9 show examples of anemometer
construction;

25 Figure 10 shows a typical anemometer calibration
curve for a zener diode anemometer;

Figure 11 is a block diagram of a simple arrange-
ment for the flow meter with analogue output fed to a
threshold alarm means (which may be remotely located);

30 Figure 12 is a circuit diagram of the zener diode
anemometer utilising a comparator for switching off the
alarm output.

The use of zener diodes in temperature measure-
ment, let alone air speed measurement, is not previously
35 known to the applicant. They are normally operated in
reverse-bias and little detail is published about their
temperature characteristics. Depending upon the individual



zener diode's breakdown voltage, the temperature characteristic is known to change in magnitude and sign.

Tests were conducted and the averaged results are graphed in Fig. 4. Each bias current was set to produce a uniform power dissipation (80 mW), to ensure substantially consistent junction temperatures. This demonstrates that the gradient is negative for a 3V device, becoming zero at about 4.7V, and increasingly positive at higher voltages. Most importantly, it can be seen that within the accuracy of measurement (10mV), a linear relationship exists.

Fig. 5 becomes a selector guide, whereby the appropriate zener diode operating voltage may be chosen according to a required temperature coefficient. A straight-line approximation to the curve yields a simple relation, the accuracy of which is largely consistent with the spread of results obtained thus far:

$$G = 1.2 \cdot (V_z - 4.6) \quad \text{or,} \quad V_z = 4.6 + (G/1.2)$$

where G is the thermal gradient (mV/°C) and V_z is the nominal voltage of the zener diode.

In view of a 15V DC supply constraint, it was decided to select nominally 8.2V zener diodes for more rigorous testing. For any given required power dissipation, the necessary bias current would be nearly 14 times less than for a regular (forward-biased) diode.

Fig. 6 shows a representative sample of numerous zener diodes tested at random. All were nominally 8.2V but two different brands are represented. The linearity and correlation was most promising, with gradients close to 4.0 mV/°C. In all cases a bias current of 10mA was used.

To take worst-case tolerance extremities, devices A and H were selected for use in the circuit configuration shown in Fig. 7(a). Fig. 7 shows that the differential output voltage (A-H) is quite linear, with virtually no change in gradient. For example when a 20°C temperature differential is applied between junctions (because the sampling element is cooled by air flow), there is virtually no change in the gradient (0.38 mV/°C becomes 0.37 mV/°C as shown).

In the case of perfectly matched devices ((A-A) or (H-H)), the differential output becomes completely independent of temperature. Unlike the thermistor situation, matching of zener diodes is a relatively simple process (because of the hitherto unconfirmed linearity of voltage variation as against temperature; and also the rugged construction).

This linearity is therein confirmed by the above test results.

The differential output voltage would normally be presented to a differential amplifier, with conventional DC offset adjustment, thence to an alarm threshold switching device (comparator).

In Summary

Under conditions of imperfectly matched zener diodes, the temperature drift relative to flow signal (differential voltage), at any ambient temperature in the range of at least 0 to 50°C, and high air flow, is 0.4%/°C. This worst-case condition represents a fourfold improvement upon the thermistor method, however, it has been surprisingly discovered the zener diodes may be relatively simply matched to whatever accuracy may be necessary to achieve any greater improvement sought by the simple process of selecting matched pairs of zener diodes.

With reference to Figure 8, construction of the anemometer circuit shown results in a sampling element such as a zener diode 10 being exposed to the air stream, and with a reference element such as a zener diode 11 substantially protected from air currents yet exposed to ambient temperature. In this arrangement, a sealed tube 13 is inserted into the wall of the pipe 12 conducting the air stream into the smoke detector (not shown). The glass hermetically-sealed zener diodes and connecting wires are mechanically and electrically secured to a printed wiring board 14 fixed within the tube 13. Bias resistors and subsequent electronic circuitry are located remotely from the tube 13 in this example. The reference element 11 is protected deep within the tube 13, whilst the sampling

element 10 projects into the pipe. Alternatively in Fig. 9 a similar result is achieved using thick-film microcircuit construction where semi-conductor elements, zener diode chips are bonded to a ceramic substrate 20, and conformally coated with a suitable protective material.

In a modified arrangement the zener diodes are operated at different bias currents. In normal operation the sampling element would be cooled by air flow. By contrast, the confined space of the reference element would lead to a rise in temperature (oven effect). Thus it is deemed appropriate to operate the reference element at a lower bias, such that in normal operation, the elements attain a similar junction temperature. Whilst the temperature characteristic is linear within the accuracy of measurement, maintaining a similar junction temperature could only improve their tracking with ambient temperature. More importantly, because the bias current is primarily determined by the sampling element in terms of overall flow sensitivity, reduction in reference bias affords an opportunity to reduce the overall current drain of the anemometer. Experimental results suggest an optimum ratio of 2:1.

Fig. 10 shows a typical anemometer calibration curve, for a zener diode design, with bias currents optimised for air speeds in the region of 1m/sec. This curve is quite linear for much of its range, simplifying the adjustment of the subsequent alarm threshold circuitry.

Fig. 11 is a schematic block diagram of the anemometer comprising compensating circuit 40 including zener diodes ZS and ZR in a resistive circuit as illustrated in Figure 12. The differential voltage output is applied to a differential amplifier 41. The output of the amplifier 41 is applied to an optional comparator 42. An analog indication of air speed is provided at the output of the differential amplifier 41, whereas the optional comparator 42 provides a set point to generate an alarm which could be used to signal excessive, or inadequate flow.

Naturally the application of this anemometer

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method is not limited to smoke detectors. It may be extended to many diverse fields of fluid flow measurement, including chemical processing, aviation, meteorology, air-conditioning, automotive, temperature measurement of fluids etc.

CLAIMS

THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:

1. A solid state anemometer comprising:

(A) a differential temperature measurement circuit including:

- i. a bridge circuit
- ii. A source of bias supply connected to opposite corners of said bridge circuit thereby to define two branches in shunt to said bias supply;
- iii. each branch having in series a current limiting resistor and a Zener diode poled so that its P-N junction is back-biased by said supply; and
- iv. means for connecting the conductor between said current limiting resistor and the associated Zener diode of each branch to respective output circuits whereat a differential output voltage can be sensed; the values of said current limiting resistors and the breakdown voltage-current characteristics of said Zener diodes being substantially identical; the voltage of said bias source being sufficient to cause a reverse breakdown of substantially equal value to flow through each of said Zener diodes, whereby when the temperature of said two Zener diodes is substantially the same over a considerable range of ambient temperatures the said differential output voltage is substantially negligible; and whereby, as the temperature difference between said Zener diodes increases over said considerable range of ambient temperatures, said differential output voltage varies substantially and correspondingly in linear relation to said temperature difference; wherein both said Zener diodes are under the thermal influence of a fluid, one of said Zener diodes being exposed to the thermal influence of a fluid flow and the other Zener diode being isolated from said fluid flow, whereby the heat developed by the reverse breakdown current through each Zener diode is dissipated differently because of the difference in fluid flow; and

(B) means for measuring the differential output



voltage, if any, existing between said diodes caused by the cooling effect of said fluid flow, if any, said measured differential being an indication of fluid flow speed.

2. The solid state anemometer of claim 1 in which the amount of current which flows through said P-N junctions of each said Zener diodes produces heat at each P-N junction of substantially the same quantity.

3. The solid state anemometer of claim 2 in which the heat produced at each P-N junction is substantially 80 milliwatts.

4. An optical air pollution monitor, said monitor including a solid state anemometer according to claim 1 which is used as an air flow detector, one of the Zener diodes of said anemometer being exposed to a fluid flow in said monitor, said fluid being sourced from an area under surveillance, the other Zener diode of said anemometer being isolated from said fluid flow but being in fluid having substantially the same temperature as the area under surveillance, said differential output voltage being an indication of continuous fluid sampling by said air pollution monitor from said area under surveillance.

5. The optical air pollution monitor according to claim 4, further comprising difference amplifier means responsive to and measuring said differential output voltage, and thereby indicating whether there is adequate fluid flow to said pollution monitor.

6. The optical air pollution monitor as claiming in claim 4 or 5, wherein said one of the Zener diodes exposed to a fluid flow is positioned in a sampling tube of said pollution monitor.

DATED this 16th day of June 1988.

MARTIN TERENCE COLE

EDWD. WATERS & SONS,
Patent Attorneys
50 Queen Street
MELBOURNE. VIC. 3000
AUSTRALIA

LJD/PNF:DD (3.6)



DRAWINGS

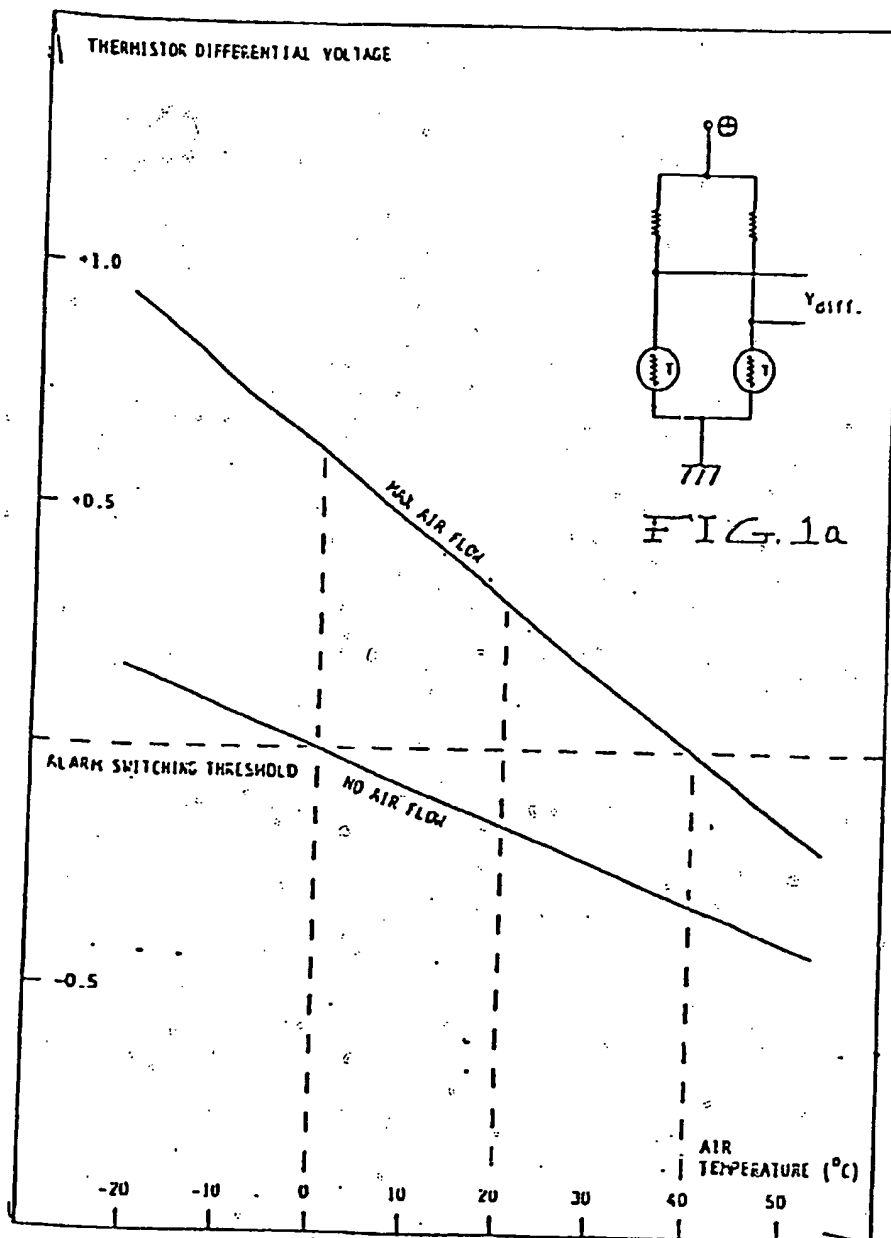


FIG. 1.

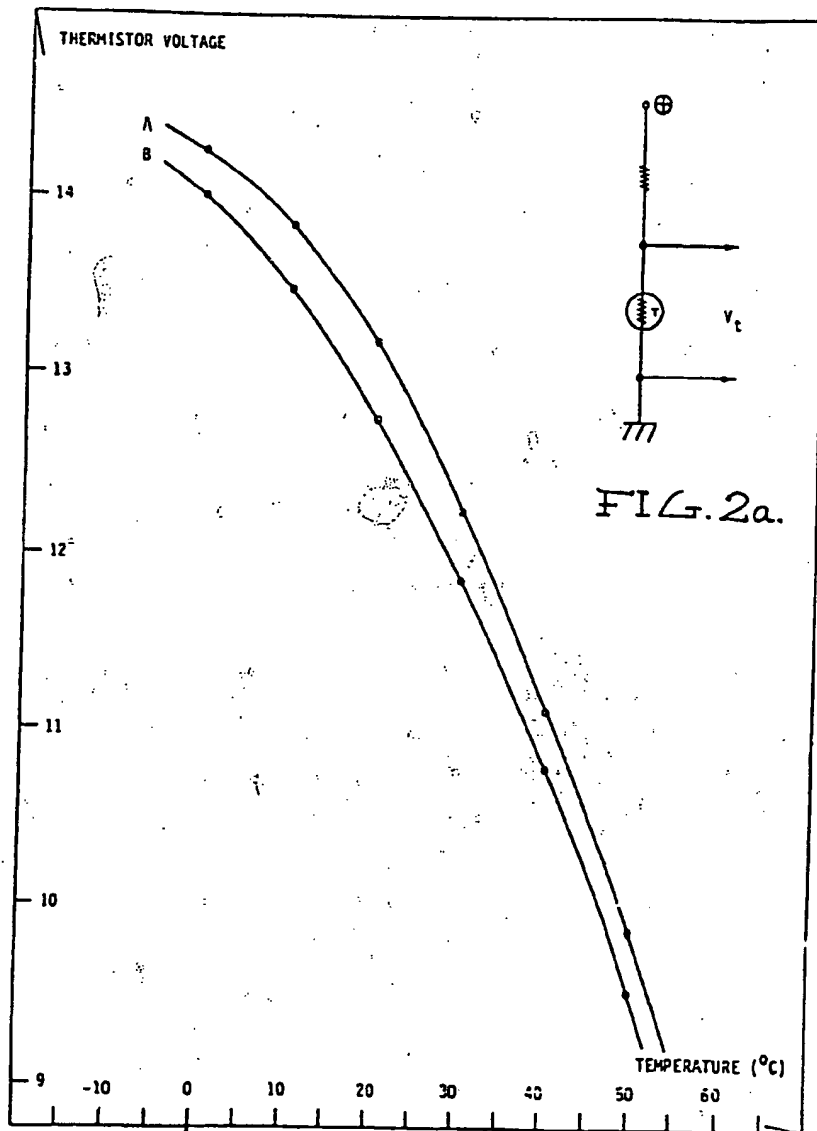


FIG. 2.

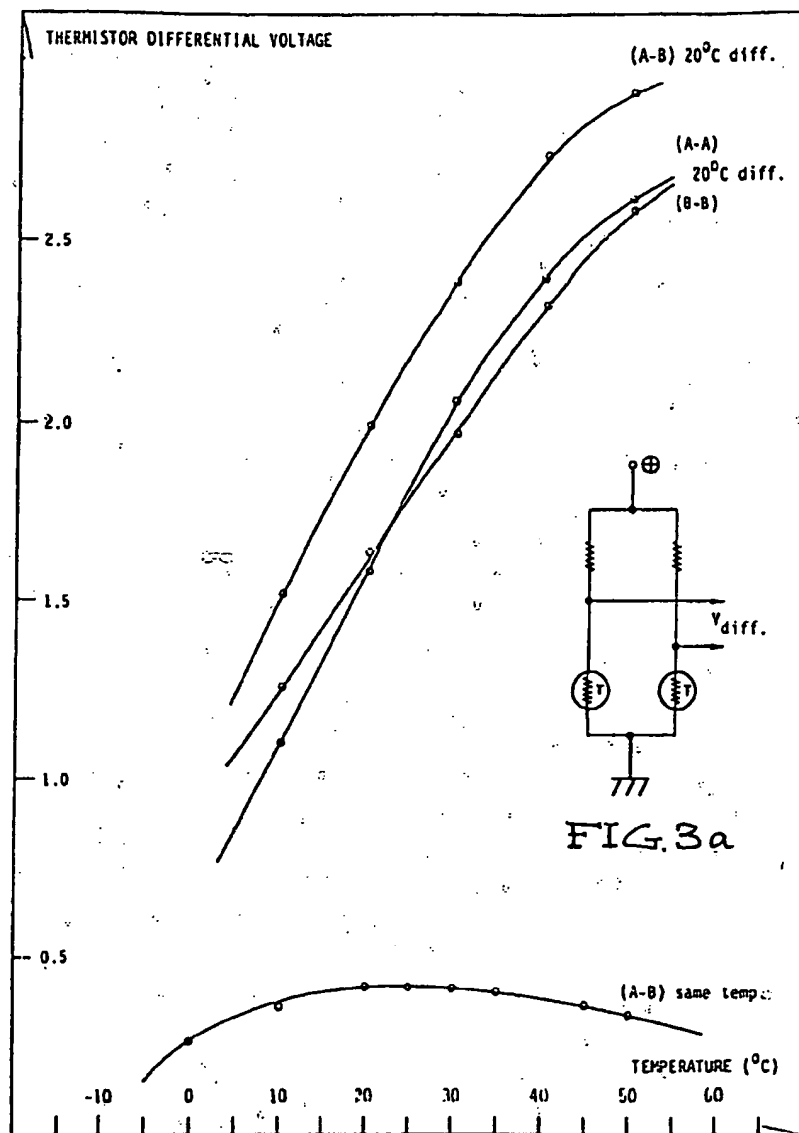


FIG. 3.

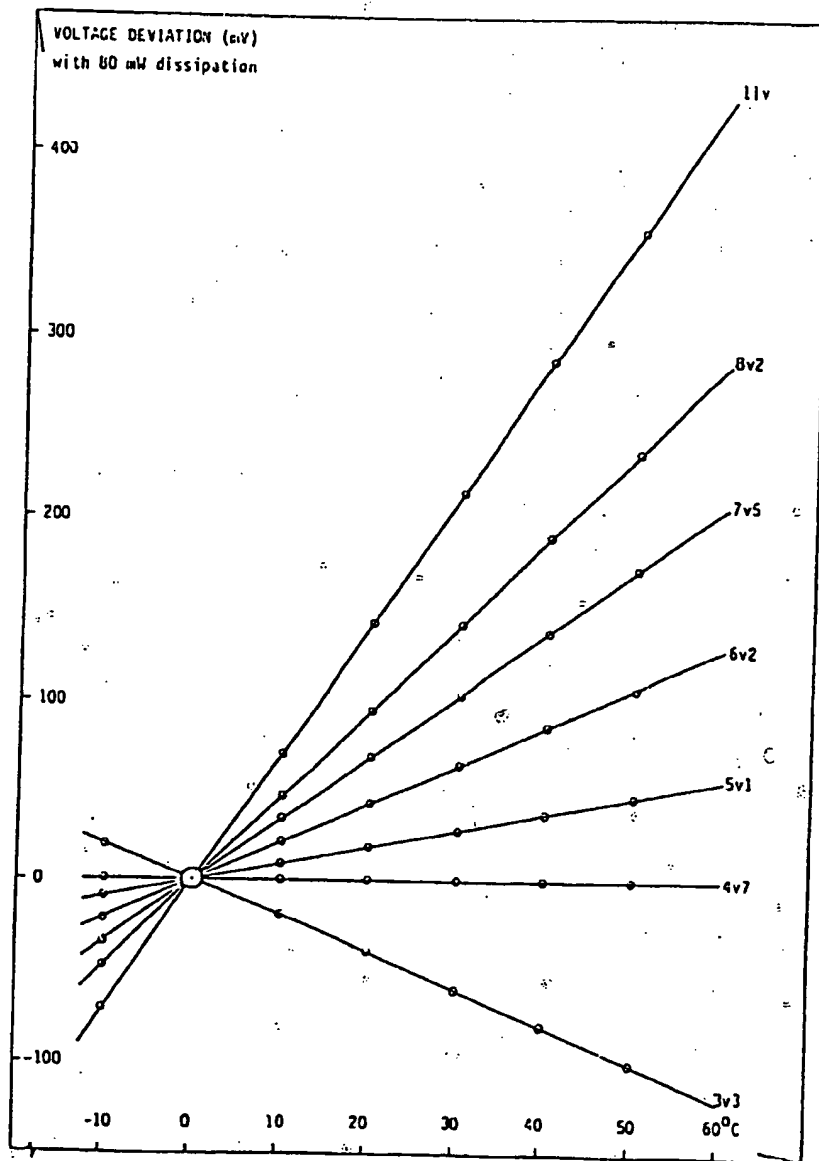


FIG. 4.

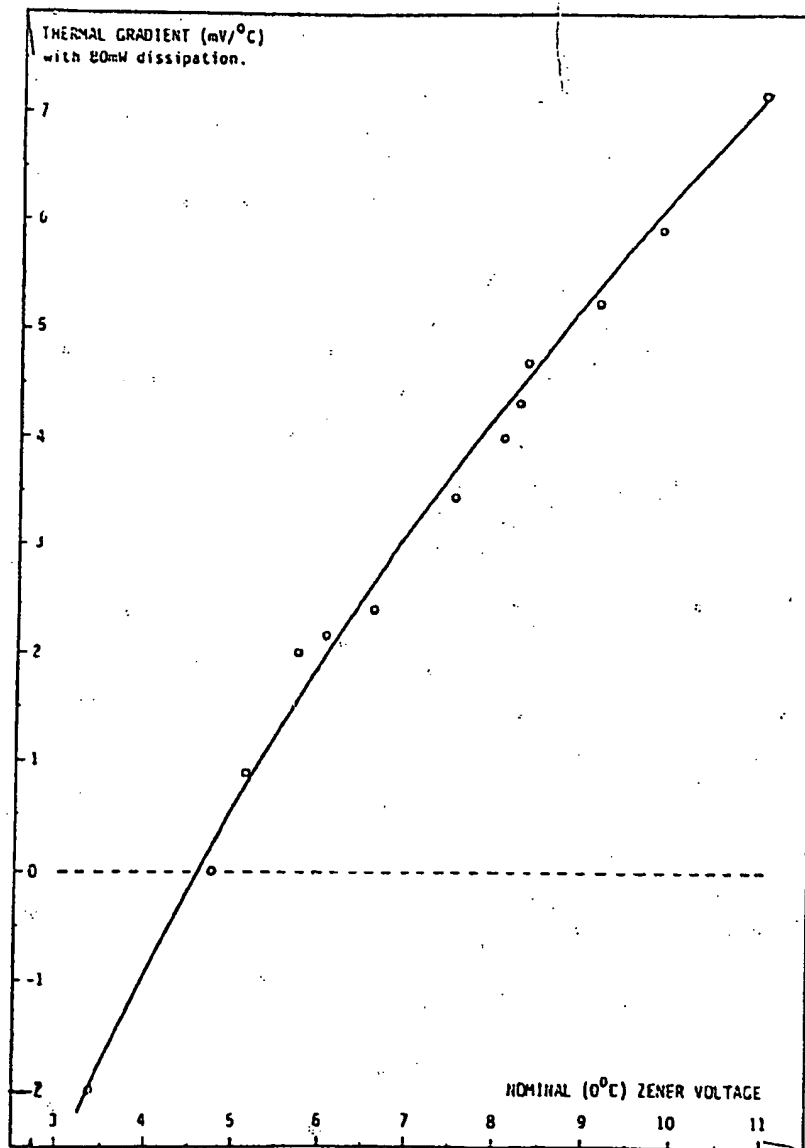


FIG. 5.

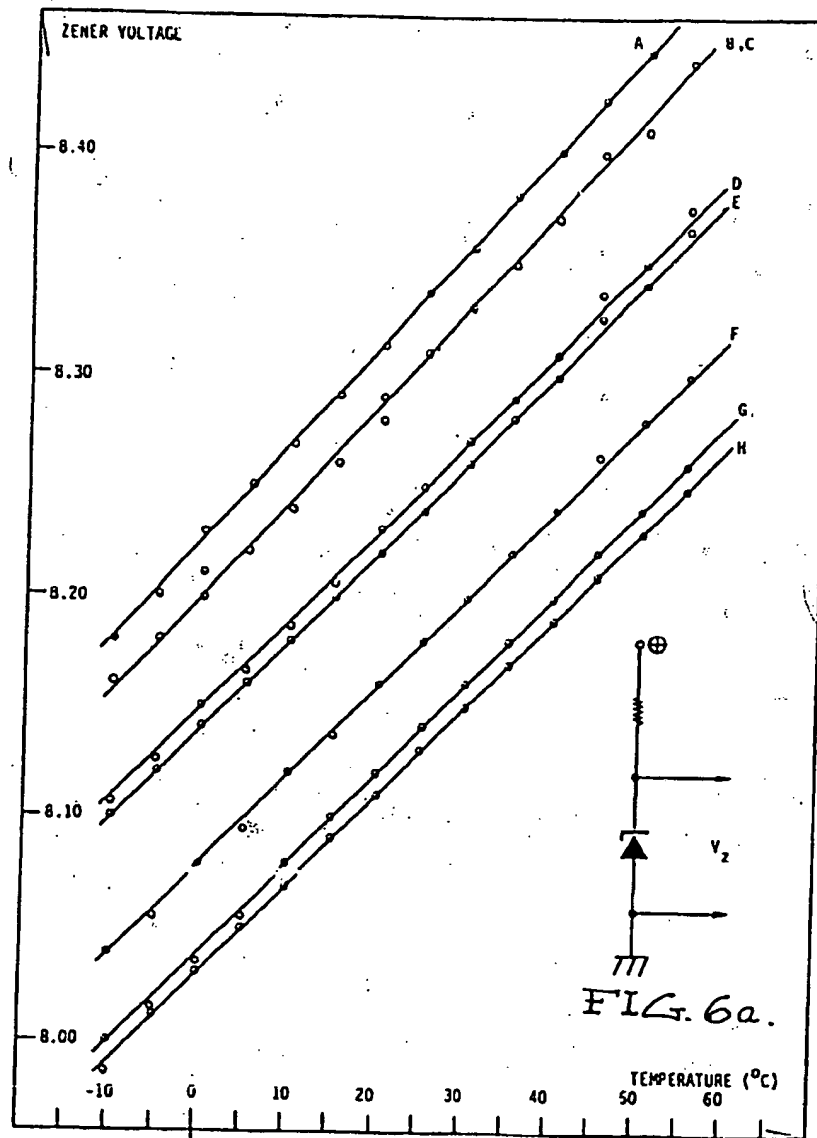


FIG. 6

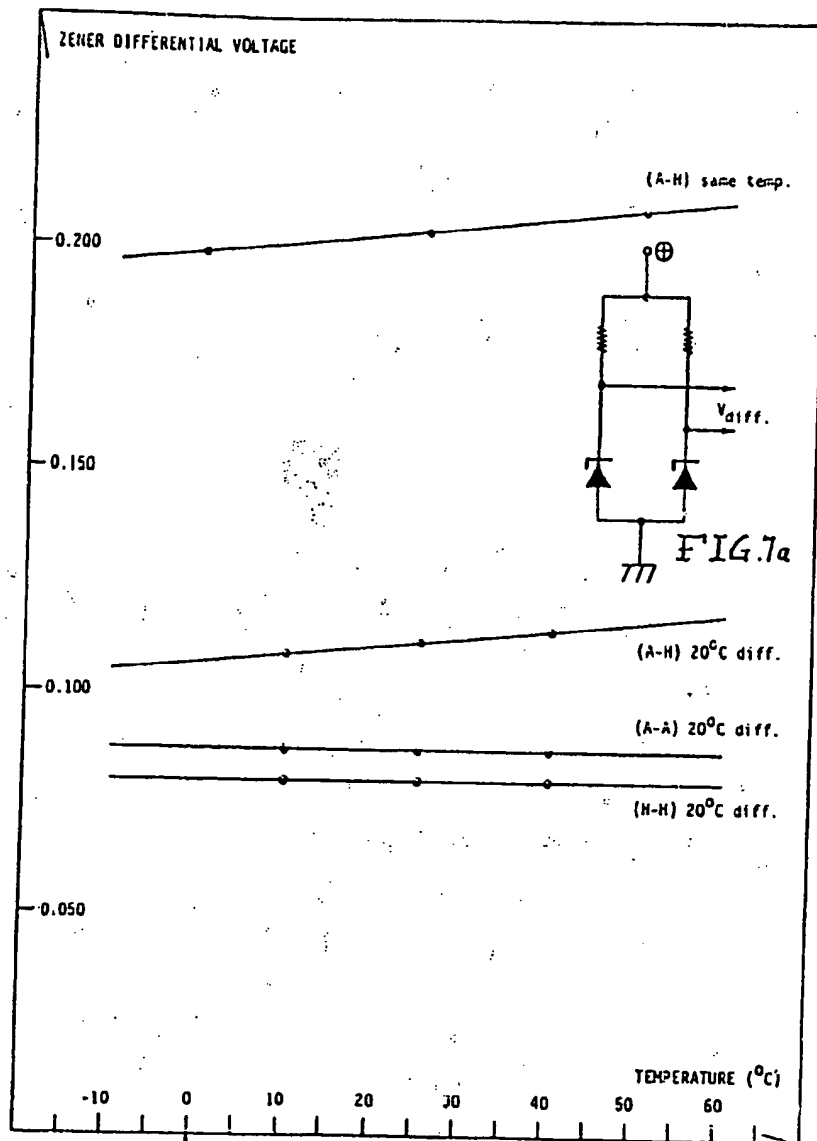


FIG. 7.

42298/85

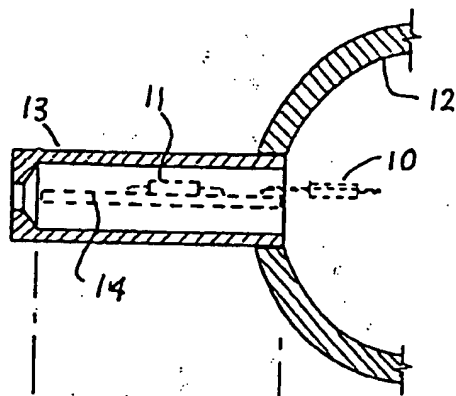


FIG. 8.

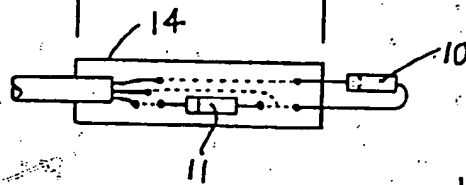
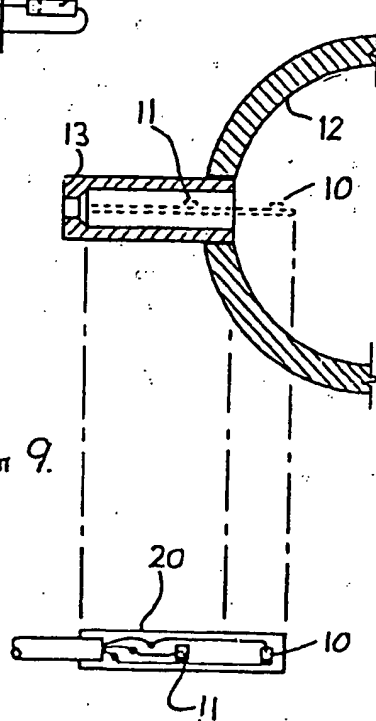


FIG. 9.



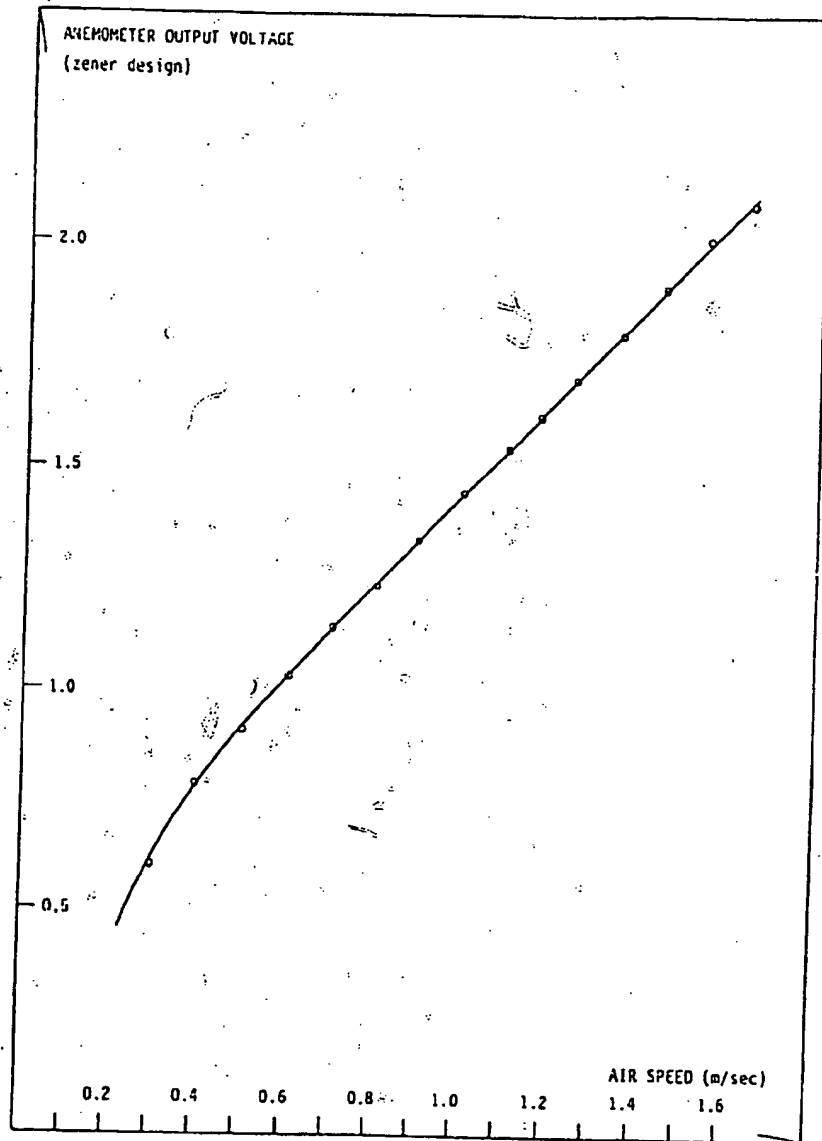


FIG. 10.

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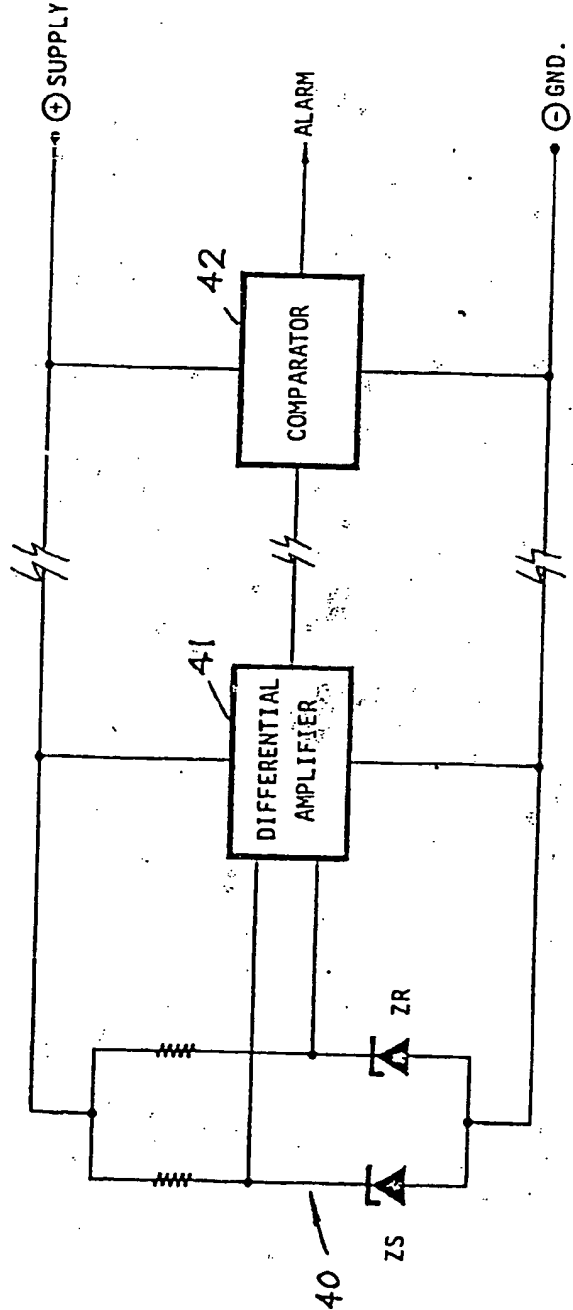


FIG. 11.

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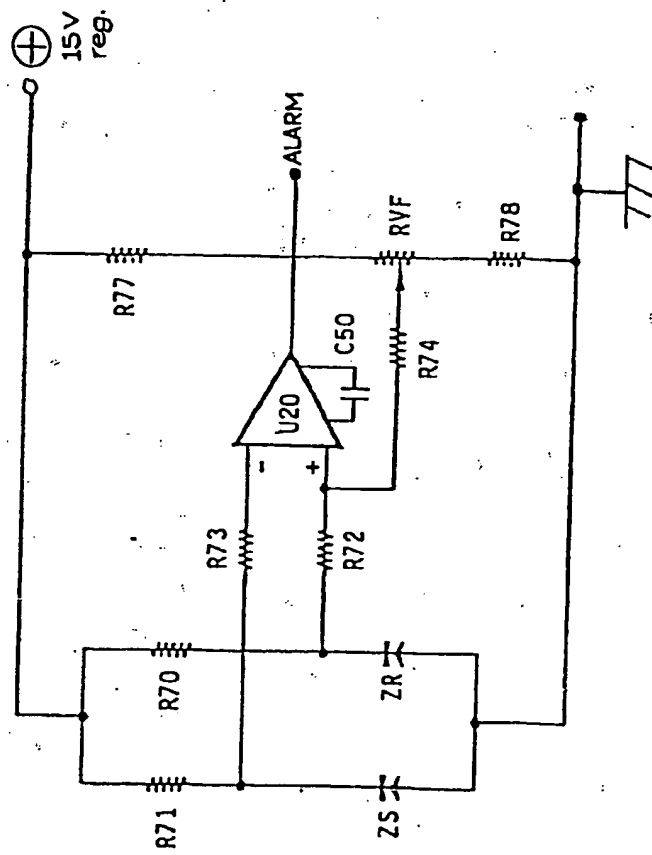


FIG. 12.

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